

## Numerical Calculation of Attenuation Mechanisms in Single-Mode Optical Fibres

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### ABSTRACT

This study presents a numerical analysis of attenuation mechanisms in single-mode silica optical fibers. The wavelength-dependent behavior of Rayleigh scattering, intrinsic and extrinsic material absorption, ultraviolet and infrared absorption, and bending losses is systematically investigated. The results show that Rayleigh scattering dominates at shorter wavelengths and decreases rapidly with increasing wavelength, consistent with its inverse fourth-power ( $1/\lambda^4$ ) dependence. Material absorption introduces pronounced loss peaks associated with hydroxyl ( $\text{OH}^-$ ) impurities, particularly near 1380 nm, which significantly limits transmission in this region. Infrared absorption increases at longer wavelengths due to vibrational modes of the silica lattice, while ultraviolet absorption decreases with wavelength and contributes negligibly within standard communication bands. Bending losses exhibit strong dependence on both bending radius and wavelength, with higher attenuation observed at smaller bend diameters and longer wavelengths. The combined attenuation profile reveals a minimum-loss transmission window in the 1300–1550 nm range, confirming its suitability for optical communication systems.

**Keywords:** Fiber optics, Rayleigh scattering, absorption, bending loss, loss coefficient.

### الحساب العددي لآليات التوهين في الألياف الضوئية أحادية النمط

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### الملخص

تقدم هذه الدراسة تحليلاً عددياً لآليات التوهين في الألياف الضوئية أحادية النمط المصنوعة من السيليكا. وتدرس سلوك تشتت رايلي، وامتصاص المادة الداخلي والخارجي، وامتصاص الأشعة فوق البنفسجية والأشعة تحت الحمراء، وفقدان الانحناء، تبعاً لتغير الطول الموجي. وتُظهر النتائج أن تشتت رايلي هو السائد عند الأطوال الموجية القصيرة، ويتناقص بسرعة مع زيادة الطول الموجي، بما يتوافق مع اعتماده العكسي على القوة الرابعة ( $1/\lambda^4$ ). ويُسبب امتصاص المادة ذروات فقدان واضحة مرتبطة بشوائب الهيدروكسيل ( $\text{OH}^-$ )، خاصة بالقرب من 1380 nm، مما يحد بشكل كبير من النقل في هذه المنطقة. ويزداد امتصاص الأشعة تحت الحمراء عند الأطوال الموجية الأطول نتيجة لأنماط اهتزاز شبكة السيليكا، بينما يتناقص امتصاص الأشعة فوق البنفسجية مع زيادة الطول الموجي، ويصبح تأثيره ضئيلاً ضمن نطاقات الاتصالات القياسية. تظهر خسائر الانحناء اعتماداً كبيراً على كلٍ من نصف قطر الانحناء والطول الموجي، حيث يُلاحظ توهين أعلى عند أقطار الانحناء الأصغر والأطوال الموجية الأطول. ويكشف منحني التوهين المُجمَع عن نافذة نقل ذات أدنى خسارة في نطاق 1300-1550 nm، مما يؤكد ملائمتها لأنظمة الاتصالات الضوئية.

**الكلمات المفتاحية:** الألياف البصرية، تشتت رايلي، الامتصاص، فقدان الانحناء، معامل الفقد.

## 1. Introduction

Optical fiber communication plays a pivotal role in the development of high-quality, high-speed telecommunication systems. In addition to telecommunication links, optical fibers are extensively utilized in the Internet and Local Area Networks (LAN) to achieve high signalling rates [1], [2], [3].

Optical fibers are generally classified as either single-mode or multimode, depending on their electromagnetic propagation characteristics. Single-mode fibers (SMFs) are distinguished by a significantly reduced core diameter—typically ranging from 8 to 10  $\mu\text{m}$ —which ensures the propagation of only a single spatial mode, effectively eliminating modal dispersion. Due to this characteristic, SMFs are the preferred choice for long-haul transmission and high-fidelity applications where signal integrity and low attenuation are paramount. Furthermore, their precision makes them indispensable in advanced medical diagnostics, including endoscopy and Optical Coherence Tomography (OCT), to achieve superior imaging resolution [4].

Multimode fibers (MMFs) are characterized by a substantially larger core diameter, typically ranging from 50 to 100  $\mu\text{m}$ . This structural design facilitates more efficient light coupling from various sources, enables the transmission of higher optical power, and permits the simultaneous propagation of multiple spatial modes. Consequently, MMFs are ideal for applications requiring high light intensity or expanded beam diameters over relatively short distances. Such properties make them particularly effective in specialized medical fields, including photodynamic therapy and laser surgery [5], [6]. Furthermore, multimode fibers significantly enhance sensing capabilities by enabling multiplexed signal detection and the parallel analysis of diverse samples. This inherent capacity for spatial multiplexing facilitates accelerated data acquisition and substantially increases system throughput. Such advantages make MMFs an instrumental component in high-efficiency sensing applications where rapid, multi-channel processing is essential [7], [8]. Despite their advantages, optical fiber communication systems encounter various attenuation mechanisms that inherently degrade overall system performance [9].

This paper aims to systematically analyze the diverse loss phenomena within single-mode fibers (SMFs)

and investigate strategies for their mitigation by employing a MATLAB program. This study evaluates these mechanisms to optimize transmission efficiency in optical fiber communication networks.

## 2. Theory Part

Attenuation in optical fibers is inherently wavelength-dependent, dictated by the physical properties of the transmission medium. In the telecommunications industry, the wavelength range of 1430–1580 nm is strategically utilized, as it aligns with the operational gain bandwidth of optical fiber amplifiers. This spectral region ensures efficient signal amplification and minimal loss over long-distance transmission [10]. Attenuation represents the loss of optical power as light propagates through the fiber medium. It is quantitatively defined as the ratio between the input power ( $p_{in}$ ), launched from the source, and the output power ( $p_{out}$ ), measured at the receiver end [11]. This parameter is critical in determining the maximum transmission distance before signal regeneration becomes necessary. The attenuation coefficient per unit length, typically expressed in decibels per kilometer (dB/km), is defined by the following relation [9], [12]:

$$\alpha_{dB} = \frac{10}{L} \log_{10} \left( \frac{p_{in}}{p_{out}} \right) \quad (1)$$

Signal attenuation is expressed through a logarithmic relationship per unit length, typically measured in decibels per kilometer (dB/km). For a fiber of length ( $L$ ) (expressed in kilometers), this loss is a fundamental parameter in system design [11], [13]. Attenuation is a critical parameter in the design of global telecommunication systems, and it is particularly fundamental in optical fiber network engineering. The degradation of the optical signal occurs due to various physical phenomena encountered along the transmission links. Specifically, as light propagates through the fiber, it suffers from intrinsic losses dictated by the chemical composition and the molecular structure of the silica material. These losses are primarily governed by the interaction between photons and the fiber's internal medium, which includes both absorption and scattering mechanisms [14].

Furthermore, attenuation mechanisms such as scattering and macro-bending losses arise from the granular and geometric characteristics of the optical fiber. The presence of metallic ions and hydroxyl  $\text{OH}^{-1}$  impurities significantly contributes to light scattering and absorption. It is essential to emphasize

that the balance between absorption and scattering is intrinsically linked to the operating wavelength, as well as the specific chemical composition of the silica glass [15], [16].

The attenuation in optical fibers is primarily governed by impurities within the silica-based medium. While photon absorption in the infrared spectrum leads to increased losses at shorter wavelengths, standard low-loss fibers exhibit an optimal minimum attenuation of approximately (0.1 dB/km) at (1.55 $\mu$ m band), this loss profile is a composite of various factors, including material absorption, scattering, mode coupling, and macro/micro-bending, as well as structural defects and radiation-induced attenuation [17].

Generally, these phenomena are categorized into three fundamental mechanisms: Scattering, Absorption and Bending.

### 2.1. Scattering Losses

In optical fibers, scattering losses originate from microscopic variations in material density, compositional fluctuations, and structural inhomogeneities or defects introduced during the fabrication process. At the molecular level, glass is characterized by a randomly distributed network of molecules [16].

The amorphous nature of glass inherently leads to localized fluctuations where the molecular density deviates—either higher or lower—from the material's average density. Furthermore, since optical glass is typically synthesized from a combination of multiple oxides, including SiO<sub>2</sub>, GeO<sub>2</sub>, and P<sub>2</sub>O<sub>5</sub>, stochastic compositional fluctuations are inevitable. These dual phenomena induce microscopic refractive-index variations on a spatial scale significantly smaller than the operating wavelength [18]. The primary origin of scattering loss is fundamentally linked to the relationship between the attenuation levels and the specific geometrical and physical parameters of the waveguide. This loss is often a direct consequence of structural imperfections inherent in real photonic waveguides [19]. In general, scattering mechanisms in optical fibers can be categorized into two main types.

#### 2.1.1. Rayleigh Scattering

The leading cause of intrinsic optical attenuation in silica fibers is Rayleigh scattering [20]. Rayleigh scattering is caused by light reflecting off of molecules in the glass whose diameter is 1/10 the wavelength of the light [21]. Rayleigh scattering arises from the inherent inhomogeneities within the

optical fiber medium. Specifically, the stochastic arrangement of molecules leads to localized density variations, which in turn cause fluctuations in the refractive index [22]. As an elastic scattering process, the frequency of the scattered light remains identical to that of the incident light [23]. This phenomenon is the decisive factor in determining transmission loss, resulting from density fluctuations that become 'frozen' into the fused silica during fabrication, creating refractive index gradients along the fiber length [24]. The intrinsic loss coefficient of the optical fiber due to Rayleigh scattering is mathematically defined as [11]:

$$\alpha_R = \frac{A}{\lambda^4} \quad (2)$$

The Rayleigh scattering coefficient A depends on the glass composition and temperature during fabrication. A in pure silica  $\approx 0.7 - 0.9(\text{dB} \cdot \text{K}^{-1} \cdot \mu\text{m}^{-4})$  [25].

The scattering coefficient A is theoretically related to the microscopic fluctuations in refractive index by the following expression [26]:

$$A = (8 \pi^3 n^8 p^2 \beta_T k_B T/3) \quad (3)$$

Where: n is the refractive index of the fiber core, p is photo elastic coefficient of silica,  $\beta_T$  is the isothermal compressibility,  $k_B$  is the Boltzmann constant, and T is the absolute temperature.

This relation shows that Rayleigh scattering increases with temperature and refractive index, and decreases sharply with the fourth power of wavelength ( $\lambda^{-4}$ ), explaining why longer wavelengths (e.g., 1550 nm) exhibit lower attenuation. In this spectral region, Rayleigh scattering constitutes the primary source of intrinsic loss. This dominance facilitates the estimation of total fiber attenuation through the characterization of Rayleigh backscattering (RBS) power levels. Consequently, the longitudinal distribution of optical power follows an exponential decay model relative to the propagation distance L, as defined by the following equation [9]:

$$p_{out}(L) = p_{in} e^{-\alpha L} \quad (4)$$

$$p_{out}(L) = p_{in} 10^{-(\alpha_{dB} L/10)} \quad (5)$$

#### 2.1.2. Mie Scattering

Linear scattering also arises from structural inhomogeneities with dimensions comparable to the guided wavelength [27], [28]. These phenomena are primarily attributed to deviations from the ideal cylindrical geometry of the waveguide. Specifically, imperfections such as core-cladding interface irregularities, longitudinal variations in the refractive index profile, diameter fluctuations, and

the presence of localized strains or bubbles contribute to this loss mechanism [29], [30].

When the dimensions of scattering inhomogeneities approach or exceed the threshold of  $\lambda/10$ , the system undergoes a transition from the Rayleigh regime to the Mie or geometric scattering regimes. In this state, the angular dependence of the scattered intensity becomes increasingly pronounced, and the total scattering cross-section may rise substantially [31].

Mie scattering, which arises from these specific inhomogeneities, is characterized by a predominantly forward-directed radiation pattern. Unlike the more isotropic distribution seen in Rayleigh scattering, this phenomenon concentrates the scattered energy along the primary axis of propagation [32]. The magnitude of Mie scattering-induced attenuation is contingent upon the fiber's material composition, geometric design, and fabrication precision. Strategic reduction of these losses can be achieved through

- (a) removing imperfections due to the glass manufacturing process.
- (b) carefully controlled extrusion and coating of the fiber.
- (c) increasing the fiber guidance by increasing the relative refractive index difference.

By these means, it is possible to reduce Mie scattering to insignificant levels [33],[ 34].

## 2.2. Material Absorption Loss

Material absorption is a loss mechanism related to the material composition and the fabrication process for the fiber, which results in the dissipation of some of the transmitted optical power as heat in the waveguide. The absorption of the light may be intrinsic (caused by the interaction with one or more of the major components of the glass) or extrinsic (caused by impurities within the glass) [35].

### 2.2.1. Extrinsic Attenuation

Extrinsic attenuation is primarily attributed to the presence of interstitial impurity atoms introduced during the glass synthesis phase. These contaminants, predominantly transition metal ions, even at concentrations as low as parts per billion (ppb) and hydroxyl ( $\text{OH}^-$ ) radicals, introduce specific electronic and vibrational absorption peaks. Notably, the ( $\text{OH}^-$ ) ions manifest as distinct absorption bands at approximately 950 nm, 725 nm, and 2700 nm, creating the well-known 'water peaks' that constrain the fiber's operational bandwidth. [36]. The intrinsic variability and non-uniform distribution of structural defects in silica fibers preclude the derivation of a universal analytical

model for absorption. Instead, extrinsic losses are typically characterized via a phenomenological approach, wherein the total absorption profile is modelled as a superposition of discrete Gaussian bands. Each Gaussian component represents the localized energetic contribution of a specific defect centre within the glass matrix, as defined by the following equation:

$$\alpha_{def} = A_i e^{-\left(\frac{\lambda-\lambda_i}{2\sigma_i}\right)^2} \quad (6)$$

Where  $\alpha_{def}$  Defect-related absorption coefficient at wavelength  $\lambda$ ,  $A_i$  Peak absorption amplitude associated with the  $i$ -th defect centre with values of 0.5, 0.6, and 0.7 dB/km, respectively.

$\lambda_i$  defines the centre wavelength of the Gaussian absorption band associated with a specific defect or impurity,  $\lambda_i$  of the Gaussian peaks are chosen to correspond to the experimentally observed absorption bands at approximately 950 nm, 1240 nm, and 1380 nm.

$\sigma_i$  is the standard deviation of the Gaussian function, which determines the spectral width of the absorption band, reflecting the extent of wavelength broadening caused by the defect distribution within the material, was selected in the range of 30–50 nm.

### 2.2.2. Intrinsic Absorption:

It is dictated by the fundamental atomic constituents of the glass matrix and establishes the ultimate lower limit for fiber attenuation [18]. This limit is defined by two physical phenomena: electronic transitions within the ultraviolet (UV) spectrum and molecular bond vibrations in the infrared (IR) region [37]. Consistent with established empirical models for silica-based media, the UV absorption edge is characterized by an exponential decay, whereas the IR tail exhibits exponential growth.

The convergence of these mechanisms creates a distinct minimum-loss transmission window in the visible-to-near-infrared range, a hallmark of high-purity  $\text{SiO}_2$  waveguides [38]. The equation used to calculate  $\alpha_{IR}$  is given by [25], [39]:

$$\alpha_{IR} = C e^{-c/\lambda} \quad (7)$$

In the numerical model, the constants C and c serve as empirical fitting parameters, the values  $C=5.4 \text{ dB.Km}^{-1}$  and  $c=7840 \text{ nm}$  are adopted to represent the infrared absorption behavior of high-purity  $\text{SiO}_2$  fibers. These values are iteratively refined to ensure high fidelity between the numerical model and the experimentally measured infrared absorption profiles characteristic of silica-based optical fibers. The equation used to calculate the  $\alpha_{UV}$ , is given by:

$$\alpha_{UV} = A_{UV} e^{\frac{4.63}{\lambda}} \quad (8)$$

Where:  $A_{UV}$  is an empirical constant (material-dependent),  $A_{UV}$  In pure silica is  $0.0261 \text{ dB.Km}^{-1}$  [39].

### 2.3. Bending Loss

Bending loss in optical fibers occurs due to structural deformations, which alter the refractive index and angle of incidence of light within the fiber core. Bending effects are generally classified into [40].

#### 2.3.1 Macro Bending Loss

Macro bending losses are triggered when a fiber is subjected to large-radius curvature, resulting in the radiation of light into the cladding. These losses often stem from unintentional physical displacements that alter the light's propagation path. As the fiber curves, the light rays deviate from the core's axis, failing to maintain total internal reflection and instead escaping into the cladding layer [40], [41].

#### 2.3.2 Micro Bending Loss

Losses arise from microscopic structural imperfections at the core-cladding interface. These defects typically result from manufacturing flaws, improper cabling processes, thermal contraction at low temperatures, or localized mechanical stress. Unlike macro bending, micro bending is significantly harder to detect because the bend radii are comparable to the fiber's core radius, leading to intermodal power coupling. These losses can be mitigated by applying a flexible protective jacket to the fiber [37], [40], [42], [43]. When a fiber is bent, the plane wave fronts associated with the guided mode are pivoted at the centre of curvature and their longitudinal. Velocity along the fiber axis. Increases with the distance from the centre of curvature. As the fiber is bent further. Over a critical curve, the phase velocity exceeds that of the plane wave in the cladding. And radiation occurs [44]. The bending-induced attenuation  $\alpha_B$  in the single-mode optical fiber was evaluated using the analytical model developed by Marcuse. The bend loss  $\alpha_B$  for a radius of curvature R is given by:

$$\alpha_B = C \frac{1}{\sqrt{R}} e^{\left(\frac{-2R\Delta V^2}{a u^2}\right)} \quad (9)$$

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2} \quad (10)$$

$$\Delta = \frac{(n_1^2 - n_2^2)^{3/2}}{n_2^2} \quad (11)$$

Where: C is a normalization factor adjusted according to fiber specifications, its approximation as  $1 \times 10^3 R$  is the radius of curvature of the fiber

bend,  $\lambda$  is the wavelength, a is the core radius of the optical fiber, u is the first zero of the Bessel function for the fundamental mode, which is approximated as  $u \approx 2.405$ .  $n_1$  is the refractive index of the fiber core and  $n_2$  is the refractive index of the cladding [45]. Table 1 shows the relevant single-mode optical fiber characteristics [46].

**Table 1:** Main characteristics of the silica optical fiber.

Optical fiber	Silica
Radius of curvature	$15 \times 10^{-3} \text{ m}$
Refractive index of the core	1.450
Refractive index of the cladding	1.445
Core radius	$6 \times 10^{-6} \text{ m}$

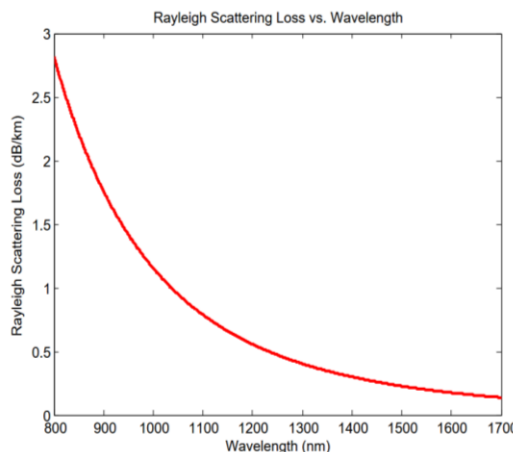
### 2.4. Total Loss

Rayleigh scattering, material absorption and Bending are three mechanisms for the fiber loss. The total attenuation coefficient is denoted as  $\alpha$  (with the units of  $\text{dB.km}^{-1}$ ). In the wavelength of 1550 nm, which is commonly used in optical communication, the attenuation coefficient is about 0.2 dB/km in the standard single-mode fiber (SMF) [47]. Considering the scattering coefficient in the range 0.12-0.16 dB/km, the total loss can be expressed as a sum of the contributions:

$$\alpha_{tot} = \alpha_R + \alpha_{IR} + \alpha_{def} + \alpha_{UV} + \alpha_B \quad (12)$$

## 3. Results and Discussion

This section presents the calculated attenuation coefficients for the optical fiber. Total attenuation is the result of several physical mechanisms, primarily material absorption, bending losses (including microbending), and scattering losses. Among these, Rayleigh scattering is a dominant factor. Figure 1 illustrates the variation of Rayleigh scattering loss as a function of wavelength, covering a range up to 1700 nm for a single-mode optical fiber. As demonstrated by Eq. (2), Rayleigh scattering exhibits a strong inverse dependence on wavelength. The results show higher attenuation at shorter wavelengths, which significantly decreases as the wavelength increases. Specifically, the loss is approximately 2.7 dB/km at 800 nm, dropping gradually to below 0.2 dB/km near 1600 nm. This trend aligns with the theoretical ( $1/\lambda^4$ ) relationship, where shorter wavelengths interact more intensely with microscopic inhomogeneities in the fiber material. Conversely, longer wavelengths, particularly within the 1300 nm and 1550 nm

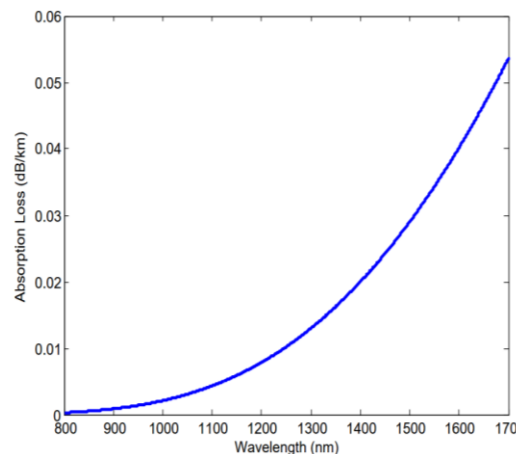


**Figure 1** Calculated Rayleigh scattering loss as a function of wavelength (nm) for a single-mode silica fiber.

telecommunication windows, experience minimal scattering. This makes these regions ideal for long-distance transmission. Overall, these findings highlight the critical role of Rayleigh scattering in defining the operational windows of modern optical systems and are in excellent agreement with established literature, e.g. [48].

Figure 2 illustrates the intrinsic infrared (IR) absorption loss in silica optical fibers was computed using an exponential decay model across a wavelength range of 800 nm to 1700 nm. As indicated by Eq. (7), the results demonstrate a clear monotonic increase in absorption loss as the wavelength shifts toward the infrared region. At shorter wavelengths, specifically those below approximately 1000 nm, the contribution of IR absorption remains negligible. However, beyond 1200 nm, the loss coefficient rises at an accelerating rate. This trend reflects the increasing influence of intrinsic vibrational absorption mechanisms (multiphonon absorption) inherent in the molecular structure of silica glass. These results are largely consistent with theoretical expectations and are in excellent agreement with established literature, such as the work of [48] and [49].

Figure 3 shows the variation of material absorption loss in an optical fiber as a function of wavelength. Unlike Rayleigh scattering loss, which decreases monotonically with wavelength, absorption loss exhibits distinct peaks corresponding to specific absorption bands. These peaks are mainly attributed to residual impurities in the glass material,

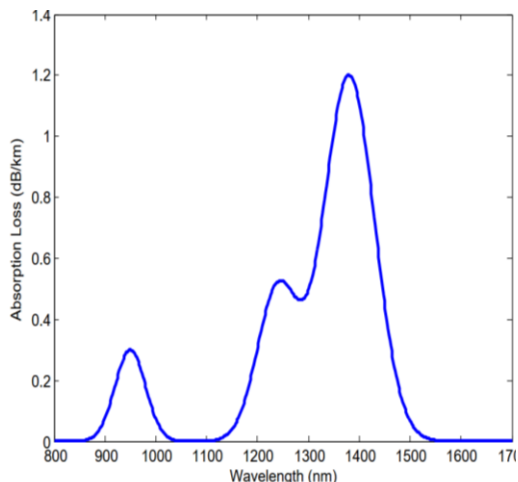


**Figure 2** Intrinsic infrared (IR) absorption loss in a single-mode silica fiber as a function of wavelength (800–1700 nm).

particularly hydroxyl ( $\text{OH}^-$ ) ions, as well as vibrational overtones of the silica lattice. As observed from Eq. (6), a moderate absorption peak appears near 950 nm, followed by a broader and more pronounced absorption band between 1200 nm and 1400 nm, reaching its maximum of approximately 1.2 dB/km around 1380 nm. This strong absorption is associated with the fundamental vibrational modes of  $\text{OH}^-$  related impurities, which significantly degrade transmission performance in this spectral region. Another smaller absorption feature can also be observed near 1240 nm, which is linked to higher-order vibrational harmonics. These absorption characteristics are crucial in defining the transmission “windows” of optical fibers. Specifically, the strong absorption around 1380 nm creates a “forbidden region” that limits efficient transmission in this range. Consequently, modern communication systems are designed to operate within low-loss windows around 1310 nm and 1550 nm, where the absorption is minimal. In summary, Figure 3 emphasizes the importance of material purity and advanced fabrication techniques in minimizing absorption losses, thereby enabling ultra-low-loss optical fibers suitable for long-haul telecommunication applications. The results obtained are found to be in good agreement with that found in the literatures, such as reference [35].

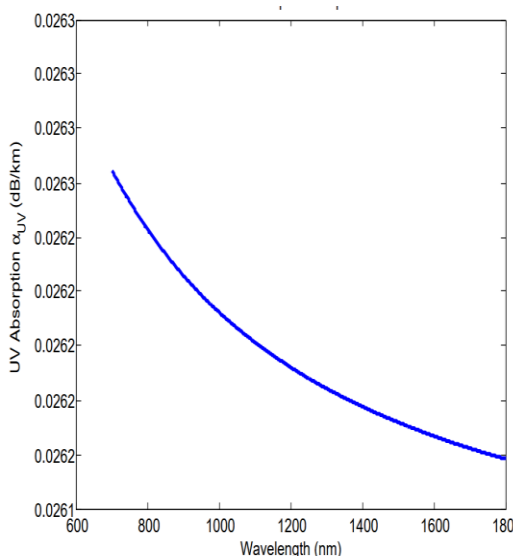
Figure 4 shows the ultraviolet absorption coefficient as a function of wavelength over a wide spectral range extending from the near-visible to the near-infrared region.

As observed from Eq. (8), the variation of the

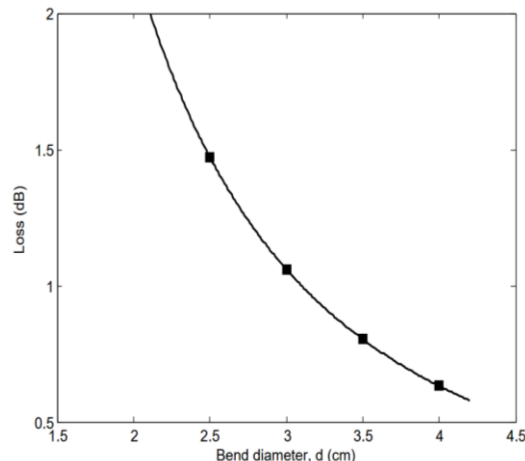


**Figure 3** Material absorption loss in optical fiber as a function of wavelength.

ultraviolet absorption coefficient with wavelength is in the range from 700 nm to 1800 nm. A gradual decrease in the absorption coefficient is observed as the wavelength increases, which is consistent with the reduced contribution of high-energy electronic transitions responsible for ultraviolet absorption. This behaviour indicates that ultraviolet absorption becomes less significant at longer wavelengths, contributing minimally to the total attenuation in the typical operating wavelength range of optical communication systems. These results are in good agreement with the results found in the literatures e.g. [1].



**Figure 4** Ultraviolet absorption coefficient as a function of wavelength in optical fiber.

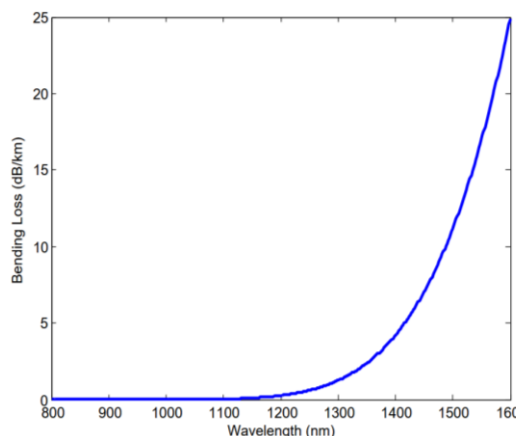


**Figure 5** Calculated macro bending loss as a function of bend diameter in a single-mode fiber.

Figure 5 gives the impact of the bend diameter on optical attenuation. As demonstrated by the calculations in Eq. (9), there is a clear and consistent trend: optical loss decreases progressively as the bend diameter increases. The results indicate that bending loss is significantly higher at smaller diameters. This is due to the sharp curvature of the fiber, which weakens mode confinement and triggers substantial radiation leakage into the cladding. As the bending radius is increased, the curvature becomes less severe, allowing the guided mode to remain more effectively confined within the core, thereby resulting in a gradual reduction in attenuation. This smooth, monotonic decrease emphasizes the high sensitivity of single-mode fibers to macro bending effects, particularly when the bend diameter falls below 3cm. These findings demonstrate that maintaining a minimum bend radius is critical for minimizing signal degradation in fiber installations. The results obtained are in close agreement with theoretical models, for example [42], [50].

Figure 6 depicts the spectral dependence of bending loss for a single-mode optical fiber, as determined by the Marcuse theoretical formulation outlined in Eq. (9). This analysis shows that as the operating wavelength rises from 800 nm to 1700 nm.

The results reveal a pronounced increase in bending loss with increasing wavelength, indicating that optical fibers become considerably more susceptible to bending effects at longer wavelengths. This behavior is primarily attributed to the reduction in optical mode confinement as the wavelength increases, which enhances radiation leakage from the fiber core under bending conditions.



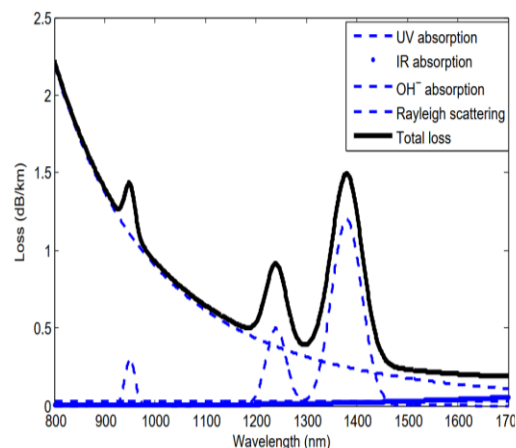
**Figure 6** Calculated bending loss as a function of wavelength (800–1700 nm) for a single-mode fiber, based on the Marcuse model (Eq. 9).

Consequently, the bending-induced attenuation exhibits a sharp rise, reflecting the exponential sensitivity of fiber losses to curvature at longer wavelengths. This phenomenon can be physically explained by the enlargement of the mode field diameter and the weakened confinement of the guided mode, leading to increased radiation loss when the fiber is bent.

The obtained results are consistent with classical waveguide theory and demonstrate that operation at shorter wavelengths significantly improves bend tolerance in optical fiber systems. Moreover, the present findings show good agreement with previously reported results in the literature, such as those presented by [51].

Figure 7 illustrates the wavelength dependence of attenuation in silica optical fibers by presenting the individual contributions of the dominant loss mechanisms along with their combined effect, as calculated using Eq. (12).

At short wavelengths (below ~900 nm), the total attenuation is dominated by Rayleigh scattering, which decreases rapidly with increasing wavelength. As the wavelength increases toward the near-infrared region, Rayleigh scattering becomes less significant, leading to a general reduction in total loss. Distinct absorption features are observed due to hydroxyl ( $\text{OH}^-$ ) impurities, appearing as localized peaks around specific wavelengths (notably near ~950 nm and ~1240 nm). These peaks indicate the strong influence of residual  $\text{OH}^-$  ions even at low concentrations, causing noticeable increases in attenuation at those wavelengths. In the longer wavelength region (>1400 nm), infrared absorption rises sharply and becomes the dominant loss



**Figure 7** Total spectral attenuation in a single-mode silica fiber, showing the combined effects of Rayleigh scattering, hydroxyl ( $\text{OH}^-$ ) absorption, and the infrared absorption tail.

mechanism, resulting in a pronounced increase in total attenuation.

The superposition of all mechanisms produces a minimum attenuation window in the range of approximately 1300–1550 nm, which explains why these wavelengths are widely used in optical fiber communication systems. Overall, the figure clearly demonstrates how different physical mechanisms govern fiber attenuation across the spectrum and highlights the importance of material purity and wavelength selection in minimizing transmission losses.

#### 4. Conclusion

This work conducted an in-depth examination of the attenuation mechanisms present in single-mode silica optical fibers. Our results show that Rayleigh scattering dominates at shorter wavelengths and decreases rapidly with increasing wavelength, while material absorption introduces distinct loss peaks associated with  $\text{OH}^-$  impurities and intrinsic vibrational modes of silica. Ultraviolet absorption was found to decrease with wavelength and contributes negligibly within the standard communication bands.

Bending losses exhibit strong dependence on both bending radius and operating wavelength, with higher attenuation occurring at smaller bend diameters and longer wavelengths due to reduced mode confinement. The combined attenuation analysis confirms a minimum-loss transmission window in the range of 1300–1550 nm, validating its suitability for modern optical communication systems. The results that are shown in this work have excellent agreement with theoretical models and

existing literature, offering practical insights for the optimization of fiber design and deployment.

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